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THERMAL IMAGING METHOD TO DETECT SUBSURFACE OBJECTS

10 This application claims priority to U.S. Provisional Patent Application
Serial No. 60/444,373, filed January 30, 2003, titled: "Thermal Inertia Imaging
Method For Remotely Sensing Subsurface Objects And Structures," incorporated
herein by reference.

BACKGROUND OF THE INVENTION

15 Field of the Invention

The present invention relates to thermal imaging, and more
specifically, it relates to a method for detecting an underground object
surrounded by a host material.

20 Description of Related Art

Dual Band Infrared (DBIR) imaging has numerous advantages over conventional thermal imaging, which utilizes only a single band. Conventional thermal imaging is difficult to interpret for three reasons:

1. It yields imprecise information that is insensitive to the subtle heat flow anomalies produced by subsurface objects.

2. It fails to distinguish between surface emissivity clutter and temperature-related heat flows.

3. Spatially-varying surface reflections (emissivity-related noise), typically equivalent to a one or two degree Celsius temperature difference, cannot be removed by using a single passive thermal IR band even when used in conjunction with another active-laser reflectance IR band.

DBIR imaging was used to detect buried land mines by exploiting temperature differences between the mine site and the surrounding soil. U.S. Pat. No. 4,005,289 describes this method, and its content is incorporated herein by reference. See N. K. Del Grande et al., "Buried Object Remote Detection Technology For Law Enforcement, in Surveillance Technologies, SPIE 1479, p. 335, 1991," which notes the difficulty of removing clutter from corrected temperature maps lacking thermal inertia diagnostics.

Thermal inertia diagnostics were used in conjunction with DBIR imaging to map flaws in heated structures (delamination gaps in bridge decks and corrosion gaps in aircraft) by exploiting thermal differences between the

flaw and the structural material. U.S. Pat. No. 5,444,241, incorporated herein by reference, describes this method.

SUMMARY OF THE INVENTION

5 By combining precise, emissivity-corrected temperature maps, thermal inertia maps, temperature simulations and automatic target recognition, the present invention provides clear clutter-free images of heated underground objects displayed in three spatial dimensions, which

1. Characterize the subsurface-object size, shape, volume, thickness,
10 depth, location and thermal inertia, relative to the surrounding host materials.

2. Provide clutter-free maps of subsurface objects displayed in three spatial dimensions.

3. Allow detection of deeper objects, at depths to twenty times the object width or diameter.

15 By combining temperature maps, obtained from imaging two different infrared wavelength bands, with inverse thermal inertia maps, obtained from imaging the day minus night, or autumn minus spring temperature spreads, the present invention exploits heat flow differences between subsurface objects and foreign-object clutter.

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BRIEF DESCRIPTION OF THE DRAWINGS

Figure 1 shows an embodiment of the method steps according to the present invention.

DETAILED DESCRIPTION OF THE INVENTION

5 A column of solid earth materials above and including a hollow object has less thermal inertia (resistance to temperature change) than an adjacent, equal-volume column of solid earth materials without the hollow object. A column of earth materials above hollow, or partially-empty objects undergo larger diurnal or seasonal temperature changes, have warmer than ambient
10 surface temperatures at midday, during autumn, and have cooler than ambient temperatures at predawn during spring. This applies to, e.g., tunnels, caves, drains, tombs, pipelines, channels, cisterns, sewers, vessels, bunkers, and trailers.

 Cumulative extraneous effects (e.g., noise produced by clutter) that can mask temperature anomalies are often an order of magnitude greater than the
15 desired anomalous component. Appropriate corrections are therefore preferably made to facilitate interpretation.

 Planck's law states that radiation emitted by a source can be related to its temperature. More precisely, Planck's law states that the radiant emittance of a surface is proportional to emissivity times absolute temperature to the power of
20 (50/wavelength in microns).

A power law thermal model provides the physical rationale for ratioing narrow IR bands involving calculating mathematical ratios using signals with equations derived from Planck's law to produce signal ratios. These signal ratios are insensitive to the natural surface emissivity and provide enhanced thermal responsivity. The derivation of this model is given in the Appendix of LeSchack and Del Grande, "A Dual-Wavelength Thermal Infrared Scanner as a Potential Airborne Geophysical Exploration Tool," *Geophysics*, VOL. 41, No 6 (December 1976) P. 1318-1336, incorporated herein by reference. In accordance with an embodiment of the present invention, this model is used to determine signal ratios that are in turn used to remove surface emissivity noise.

The emissivity of surface materials is highly variable from one land area to another. However the ratio of signals at two or more wavelengths can be used to obtain highly precise surface-temperature measurements that depend very little upon emissivity variations. For example, temperature differences as small as 0.2 degrees C can be obtained by using the present invention.

At wavelengths where the radiation has the same spectral slope as a blackbody source, i.e., an object that absorbs all radiation, the emissivity ratio variations are very small. Thus, in an aspect of the invention, quantitative temperature measurements are made using signal ratios that are calibrated against a standard blackbody source.

A typical greybody surface is an object that absorbs about 95-99% of all radiation and thus has an emissivity of less than 1. If a structure is a greybody, its respective temperatures will look alike at wavelengths of 5 micrometers and 10 micrometers.

5 Where the surveyed structure behaves in true greybody fashion, no matter what area is scanned, the ratio of emissivity at one wavelength divided by the emissivity at a second wavelength $\epsilon_{\lambda_1}/\epsilon_{\lambda_2}$ is constant. The ratio of two signals at differing wavelengths can then be calibrated and the blackbody temperature obtained. In one aspect of the present invention, $\lambda_1 = 5 \mu\text{m}$ and $\lambda_2 = 10 \mu\text{m}$,
10 respectively, because these are the common wavelengths that are recorded by present-day scanners.

 Because the heat flow anomaly is difficult to accurately measure, corrections may be made to accurately associate the thermal anomaly with a subsurface object. Furthermore, measured surface temperatures can be
15 inaccurate because of an emissivity factor (noise) generated by clutter. Clutter may include, e.g., shadows, tracks, stains, disturbed terrain, holes, vegetation, foreign objects, foreign materials, foreign soils, water, cool air pools and roughness variations.

 Clutter of a specular nature may be identified and removed by image
20 processing because it has a distinctive emissivity signature. The emissivity factor produced by reflected-infrared signal noise, relates to the ability of surfaces

which produce clutter to emit radiant energy less than that of a black body at the same temperature and differently at one wavelength than at another. A black body is an ideal surface that absorbs and emits all radiation without reflection.

The present invention provides a method for detecting an
5 underground object surrounded by a host material, where the detection is accomplished by using thermal inertia diagnostics, which removes both surface and subsurface foreign-object clutter. The host material is analyzed using visible, temperature and thermal inertia imagery to characterize the contrasting features of the host material from those of the object. An area of the structure is then
10 scanned simultaneously at two or more different wavelengths of radiation to produce a time sequence of images taken at different times during day and night or at different months during the year. The time sequence of images is processed into signal ratios that are used to remove clutter.

Obtaining a temperature versus time history is important to determine
15 the size, shape, volume, depth, type and location of the object. Despite the elimination of clutter of a reflective nature, images cannot be interpreted very easily without also studying the time history of infrared image ratios, which eliminate clutter of a thermal nature.

Other informative maps may be generated by repeating temperature
20 survey measurements at two or more different times when the diurnal or seasonal temperature spreads provide the greatest contrast for the object and

host material, compared to subsurface foreign objects and foreign materials which produce thermal-image clutter.

Thermal image clutter may be identified and removed by mapping the maximum minus the minimum temperature spread from coregistered day minus
5 night, or autumn minus spring, temperature maps. Thermal image clutter is produced by foreign objects, and materials, such as: disturbed terrain, animal holes, roots, water, mud and rocks which resist diurnal and seasonal temperature changes differently than the sought-after object and host material.

The diurnal or seasonal temperature spread provides a unique
10 signature to identify and remove thermal image clutter when combined with the different location, size, shape, volume, depth, and inverse thermal inertia which distinguishes foreign objects and materials from the targeted object.

Further in accordance with an embodiment of the present invention, the corrected temperature data is used to generate corrected temperature and
15 temperature-spread maps. Corrected temperature and temperature-spread maps are color-coded images that show color patterns of conducted heat generated by objects which heat and cool at different rates relative to the surrounding materials. These patterns are distinguished from the patterns produced by foreign objects, materials and structures.

20 The interpretation of the images is improved by removing the clutter and thus increasing the signal to noise ratio. As a result, corrected images are

formed, thereby facilitating the removal of heat flow anomalies associated with subsurface clutter.

Automatic target recognition may be used to remove reflective signal clutter from infrared signals which produce emissivity-noise, For example, maps
5 are overlayed related to temperature, T, and emissivity ratios, R, from Equations 1, 2, 3 and 4, from U.S. Patent No. 5,444,241, incorporated herein by reference, for dualband infrared wavelengths detected at 5 and 10 micrometers.

$$T = [I_5 / I_{10}] / [I_5 / I_{10}]_{Average} \quad (5)$$

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$$T = [(\epsilon_5 / \epsilon_{10})(T)^5] / [(\epsilon_5 / \epsilon_{10})(T)^5]_{Average} \quad (6)$$

$$R = [(I_{10})^2 / I_5] / [(I_{10})^2 / I_5]_{average} \quad (7)$$

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$$R = [(\epsilon_{10})^2 / \epsilon_5] / [(\epsilon_{10})^2 / \epsilon_5]_{Average} \quad (8)$$

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Reflective signal clutter detected at co-registered T sites where R sites that are not within plus or minus two standard deviations from the average R value are removed and replaced with an average value. The result is a corrected temperature map.

To remove thermal signal clutter from heat flows unlike heat flows associated with the object or host material, a comparison is made of the measured relative temperature spread contrast ΔT_m with the calculated relative temperature spread contrast ΔT_c . The relative temperature spread contrast is
5 obtained by overlaying and subtracting co-registered temperature maps taken during day and night, or autumn and spring.

Calculated relative temperature spreads, ΔT vary inversely as the thermal inertia, P , or resistance to temperature spread, and directly as the fractional volume, f of the object, (o), and $1-f$ of the host, (h) for a column of unit
10 area and unit volume. The relative temperature spread contrast ΔT is calculated for column 1 with the host material and the object minus column 2 with the host material only, divided by the temperature spread of the host material only column.

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$$\Delta T = [(\Delta T)_o + (\Delta T)_h] / [(\Delta T)_h] \quad (9)$$

$$\Delta T = [(f/P_o) + (1-f)/P_h - 1/P_h] / [1/P_h] \quad (10)$$

$$\Delta T = f[(P_h)/(P_o)) - 1] \quad (11)$$

All measured ΔT_m sites which do not fall within specified limits of the calculated ΔT_c of about 50 for typical hollow objects, embedded in solid host materials, at depths twenty times their diameter are removed and replaced with an average value.

5 An embodiment of the process steps of the present invention is provided in Figure 1. A selection is made of a host and a subsurface object site environment (10). Note that the host and subsurface object site environment are naturally heated, not artificially heated. A survey is carried out of the host and said object site by: simulating the temperatures of said host and said object site
10 (12), calculating the thermal inertias of said host and said object site (14), and computing the temperature spreads (e.g., twice-daily and bi-yearly) of the host and said object site (16). A determination is made whether the thermal inertia of the object site is distinguishable from that of the host (18). A change is made of the environment of the host and the object site if the temperature spread of the
15 object site is not distinguishable from that of the host (20). The previous steps are repeated until the object site is distinguishable from that of the host (18). The host and object site are then scanned at different times with two different IR wavelengths (22) and a spatial sequence is recorded of dual-band IR images at different times (24). A record is made of the object and host temperature,
20 thermal inertia and temperature spread (26). A calculation is made, on a computer workstation (28) using image-processing code (30) of signal ratios and

differences to form temperature, emissivity-ratio and corrected-temperature maps. Emissivity, temperature and temperature-spread maps are then coregistered (32). Temperature maps and temperature-spread maps are then corrected (34). Foreign object thermal clutter is removed from the temperature-spread maps (36). Object location, size and shape are determined from the temperature maps (38). Object thickness, volume, and depth information are obtained from said temperature-spread maps (40). Object location is determined (42) and a 3D display of the object is provided (44).

A unique aspect of the present invention is the realization that thermal inertia contrast can be located for solid or semi-solid objects by detecting disturbed, moistened or displaced earth materials, which surround them. For example, this applies to subsurface walls, foundations, aquifers, ditches, burial sites, landmines, munitions, leaky pipelines and foxholes.

Another unique aspect of the present invention is the realization that thermal inertia contrast can be located for hollow, or partially empty structures by detecting undisturbed, or compacted earth materials, which surround them. For example, this applies to contained, hollow or partially empty tunnels, caves, drains, tombs, pipelines, channels, cisterns, sewers, vessels, bunkers, and trailers.

Using airborne infrared imaging from an unmanned airborne vehicle, an ancient rock-hewn drain was located under the Dome of the Rock platform, in Jerusalem, Israel. The drain image was recorded at 1:00 am on September 22,

2002. Environmental conditions were optimum. The ratio of thermal inertia (resistance to temperature change), for equal volumes of limestone and air is 785 to 1. In summer, the trapped air within the drain stores excess heat, which conducts slowly to the surface. This allows the drain to be detected at depths
5 over ten times the 3.2 meters (10.5 feet) drain width.

The shallow drain end is less than 1 meter (3.3 feet) deep, north of the Dome of the Rock. The deep end of the 136 meter (446 feet) long drain, is over 15 meters (49 feet) deep, as it descends under the Large Cistern, at the southeast corner of the Dome of the Rock platform.

10 Another unique aspect of this invention is the realization that the thermal contrast can be detected, between typical contained, hollow or partially-empty structures, which have approximately three orders of magnitude less thermal inertia (equal to the square root of the product $k\rho C$, for k = thermal conductivity, ρ = density and C = heat capacity) than the surrounding
15 undisturbed earth. For example, this applies to contained, hollow or partially-empty tunnels, caves, drains, tombs, pipelines, channels, cisterns, sewers, vessels, bunkers, and trailers.

While particular embodiments of this invention have been shown and described, it is readily understood that numerous modifications may be made to
20 the method that would fall within the scope of the appended claims. For example, the wavelength ranges selected for scanning may be varied. Moreover,

additional corrections to images (representing surface temperature and surface emissivity) may be made depending on the environment in which a particular structure is exposed to, i.e. pollution, dust, acid and other conditions.

The foregoing description of the invention has been presented for purposes of illustration and description and is not intended to be exhaustive or to limit the invention to the precise form disclosed. Many modifications and variations are possible in light of the above teaching. The embodiments disclosed were meant only to explain the principles of the invention and its practical application to thereby enable others skilled in the art to best use the invention in various embodiments and with various modifications suited to the particular use contemplated. The scope of the invention is to be defined by the following claims